

# ***Reduction of Development Costs of Full Composite Aero-Structure :A Proposal from a Research Sector***

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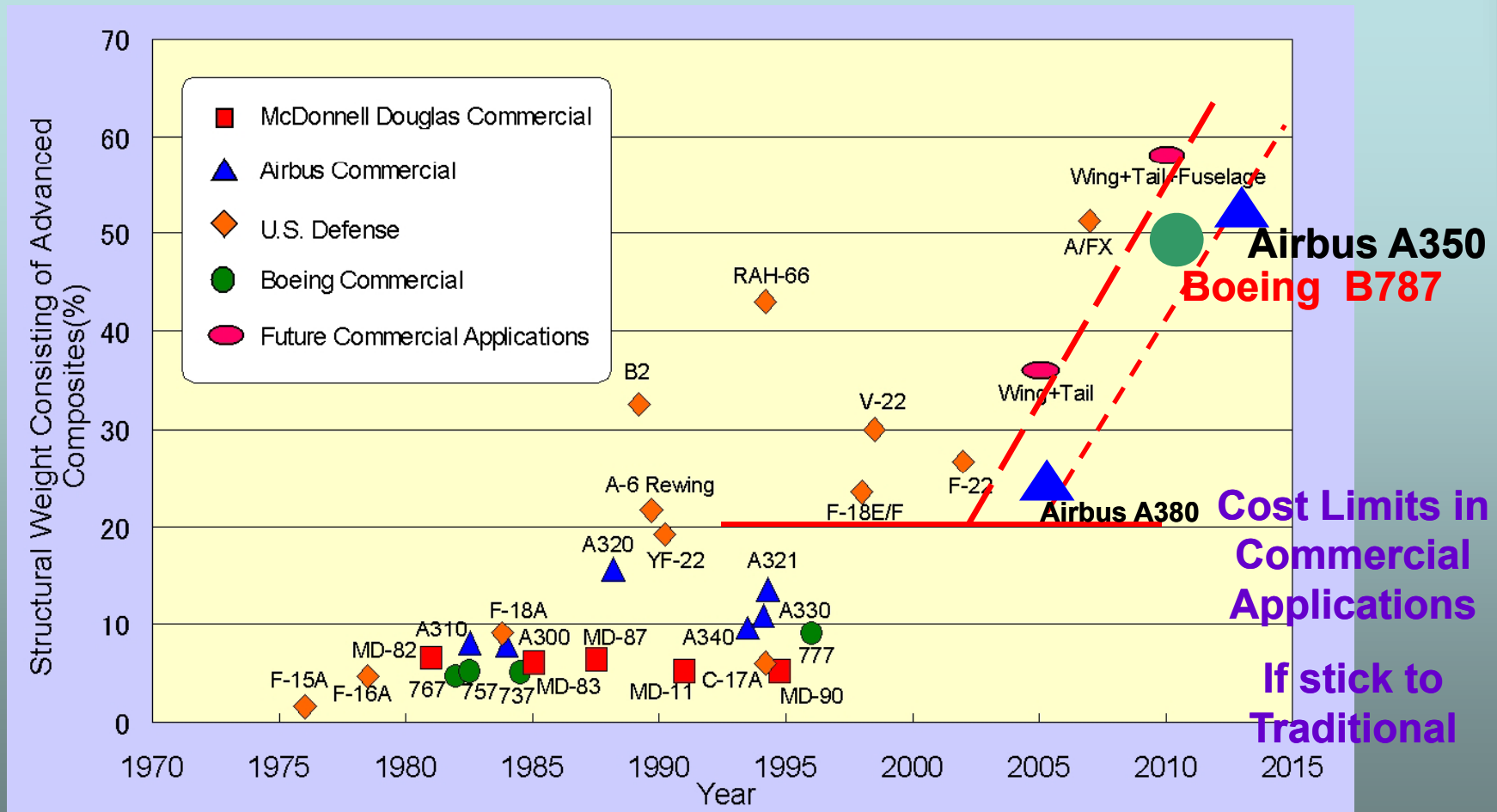
B-787 First Wing Roll-Out: Courtesy of Website of Mitsubishi Heavy Industries Co. Ltd.

# Outline of the Presentation



- Increase of composites percentage in aero-structures
- **Recent two major challenges: B-787 and A350**
- Precious lessons learned: Delay and cost issues,  
Unexpectedly low weight reduction, increase?
- **Proposal for Development Cost Reduction**  
Substitution of some steps in BBA by “Virtual testing”  
Essential difficulty: Progressive failure simulation  
Reduction of trial fabrication by “Virtual processing”  
[ Out of scope, today ]
- **Example: Lower panel test of VaRTM wing, predictable**
- **Example: Lightning strike damage, only at gateway**
- **If fails, industries may return to aluminum structures**
- **Conclusions**

# History of Composites Application to Aircraft





# Two Major Challenges to Full Composite Aero-Structures A Case of Boeing B-787



**Picture of B-787 in ANA Painting**  
(Courtesy of New Release of Boeing Japan: May 26/2011)

**Pictures of B-787 at  
Farnborough Air Show in 2010**



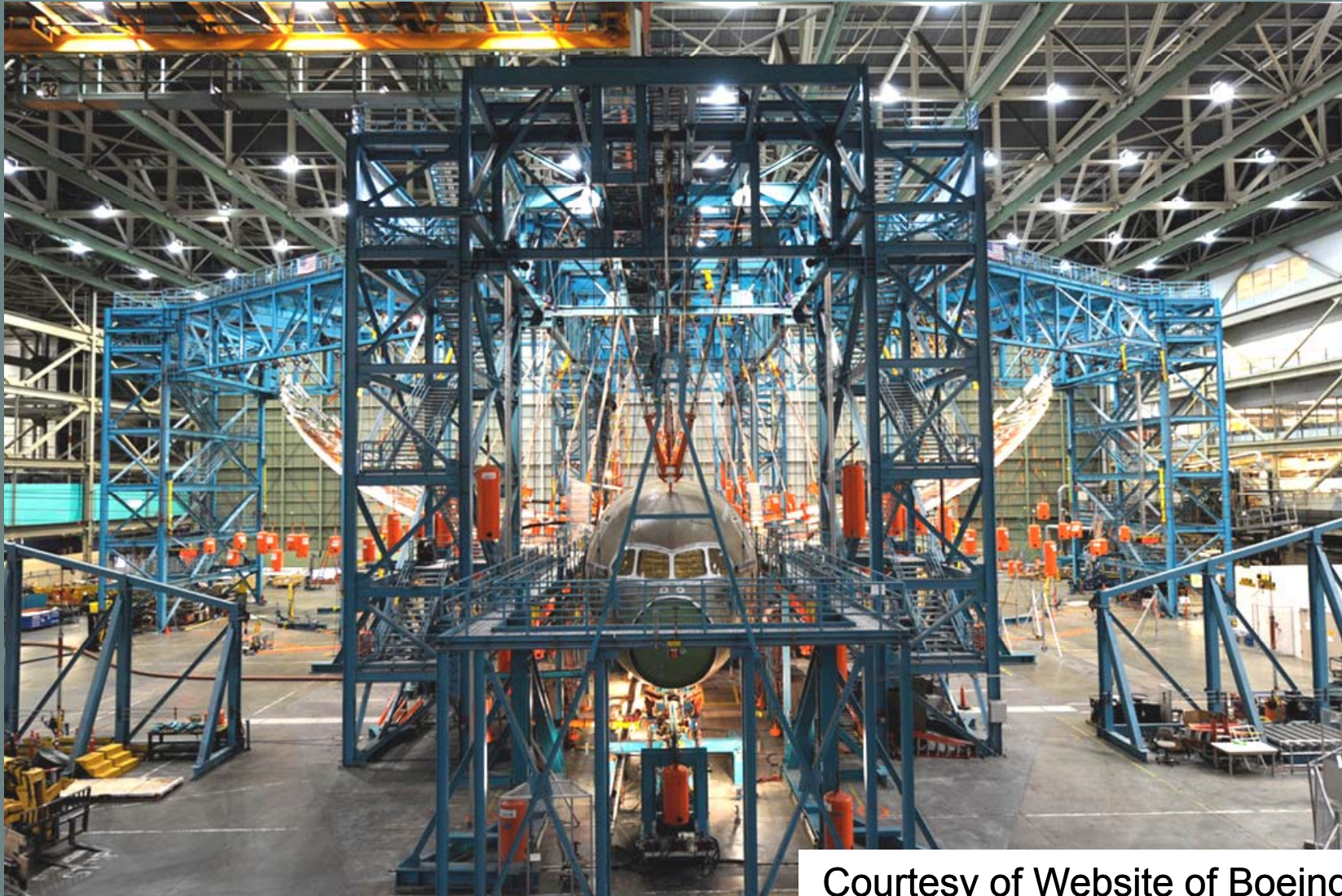
# Picture of B-787 Main Wing at Roll-out Ceremony at MHI O-e Plant



Courtesy of Website of MHI Co. LTD

**Using Toughened Epoxy Prepreg:  
Auto tape lay-up machines are used  
in lamination process of wing skin**

# Successful Design Ultimate Test of B-787 Main Wing



Courtesy of Website of Boeing Co.



# Picture of Full Composite Fuselage of B-787



**Demo Parts:**  
In the production,  
Work share by  
Kawasaki Heavy  
Ind. (KHI), Japan  
and Alenia, Italy.

**Precious Lessons Learned**  
**▲ Difficulty in the processing**



**Great Advantage of Composite Fuselage**

- **Absolutely No Corrosion**
- **Contribution to Passenger Amenity**

# Two Major Challenges to Full Composite Aero-Structures A Case of Airbus A-350 XWB

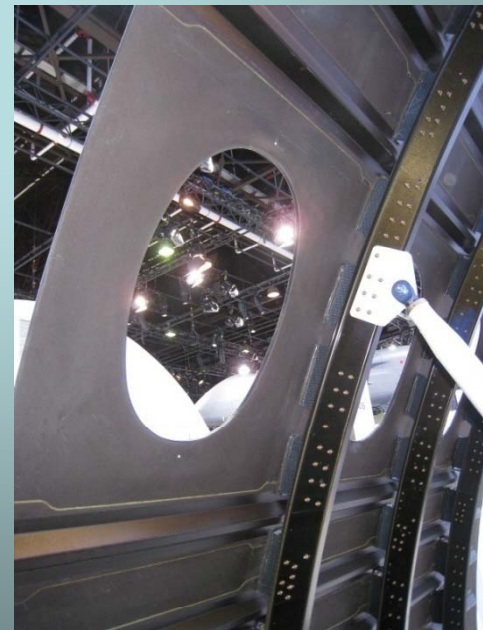
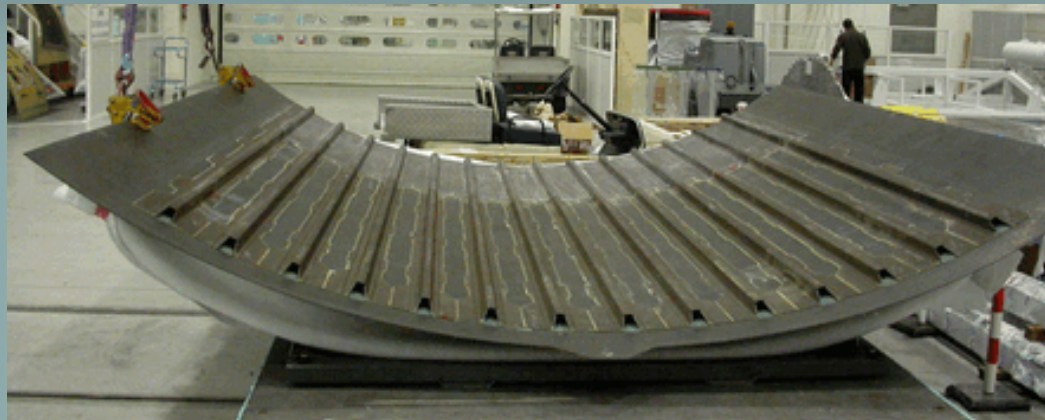


© Airbus Proprietary



# Full Composite Fuselage of A350 XWB

above: Upper Panel, below: Demo Parts of Side Panel



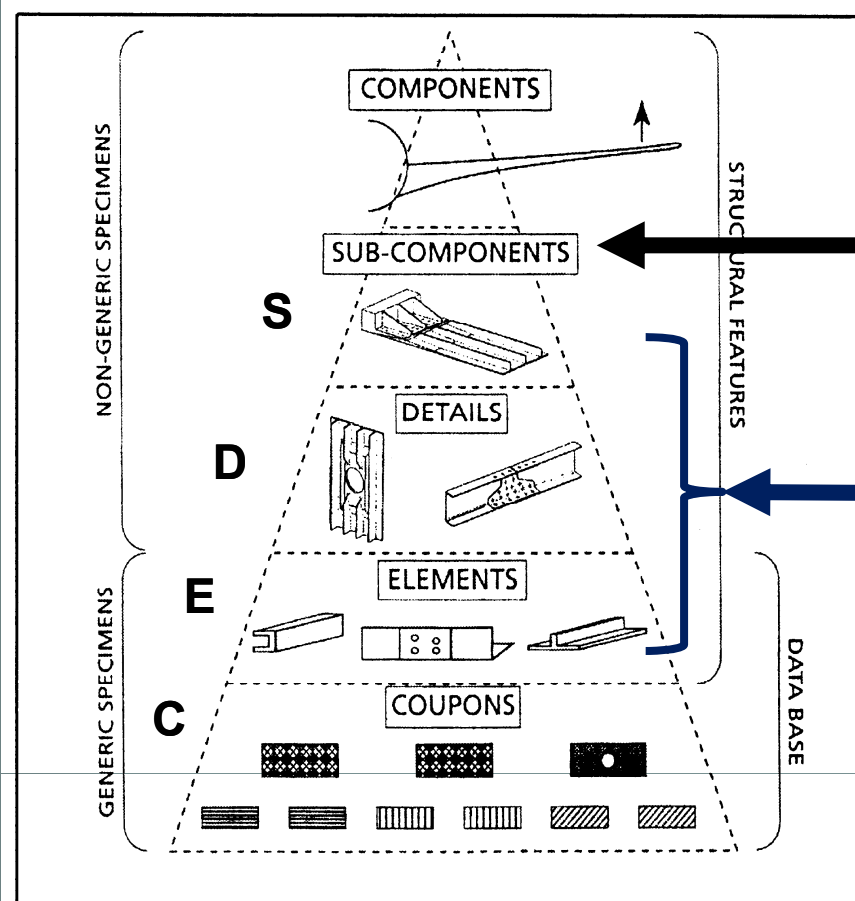
**Lessons Learned: Delay of Development, Cost Issues?**

# Proposal for Development Cost Reduction of Full Composite Aero-Structure

- ***Substitution of Some Steps in Building Block Approach by High Accuracy Numerical Simulation of Tests [Virtual Testing]:  
Consideration of Damage Propagation in the Failure Process = Essential Point***
- ***Reduction of Trial Fabrication by High Accuracy Numerical Simulation of Processing [Virtual Processing]:  
Out of Today's scope***

# Established Procedure of Type Certification of Composite Aero-Structure Building Block Approach (BBA)

BBA is considered as inevitable approach. However, as a research sector, two questions can be raised.



## Two Basic Questions

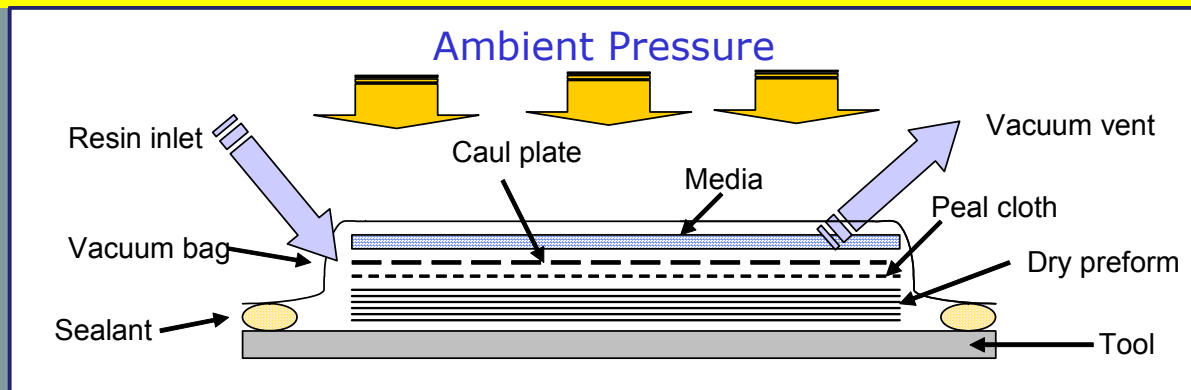
1. Sub-Components must be close in size to "Components"?
2. Some steps like elements and details can be replaced by numerical predictions?

**"Virtual Testing"**

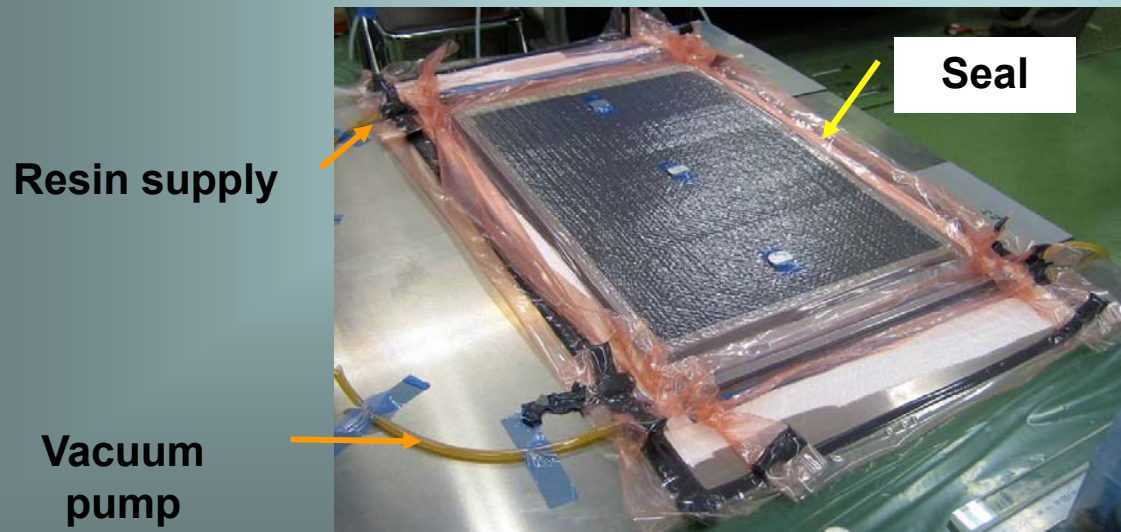
# JAXA pursues Development of VaRTM Composite Aero-Structures



## Outline of technology for Low Cost Composite Manufacturing



**VaRTM : (Vacuum assisted Resin Transfer Molding)**



A Good Example  
of Virtual Test for  
Predicting  
Damage  
Propagation

Shown in this Color  
Bar Slide

# Fabrication of 6m Full Size Panel

(Bagging and vacuuming)



Heat Insulation Panel



Needless costly autoclave!

Fan heater blower

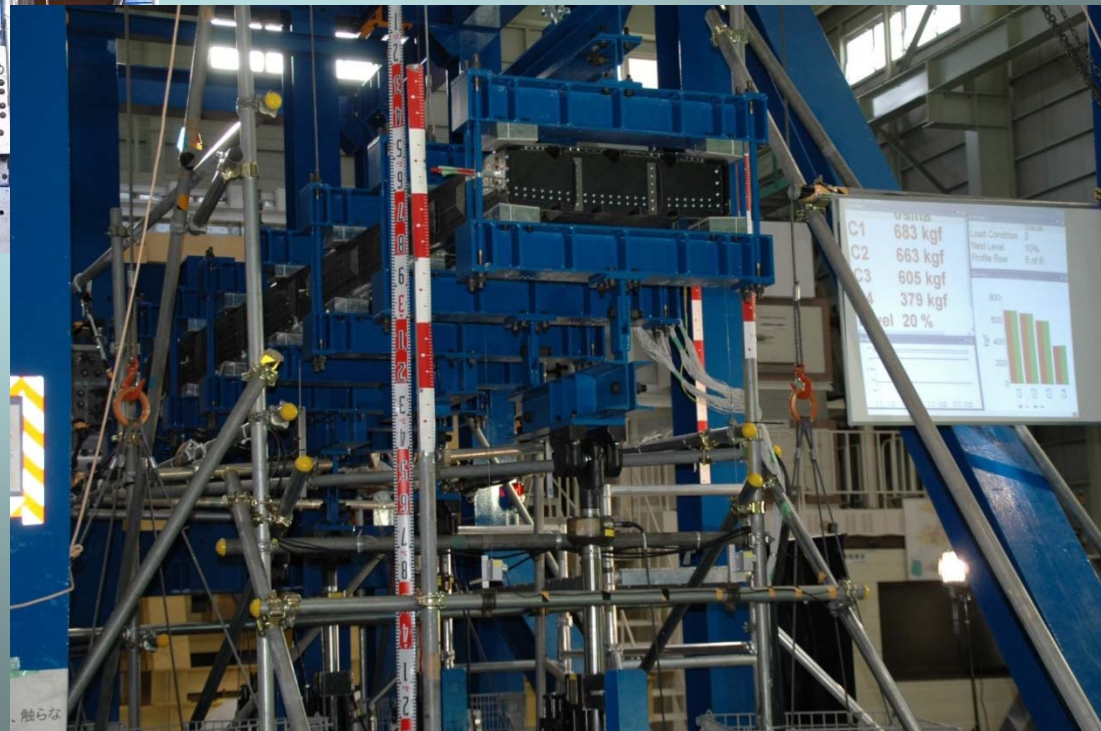
**Simulation of Fabrication Process =  
Virtual Processing: One Point of Proposal  
Omitted in Today's Presentation**

# 6m Full Size Wing Box in the Test Rig

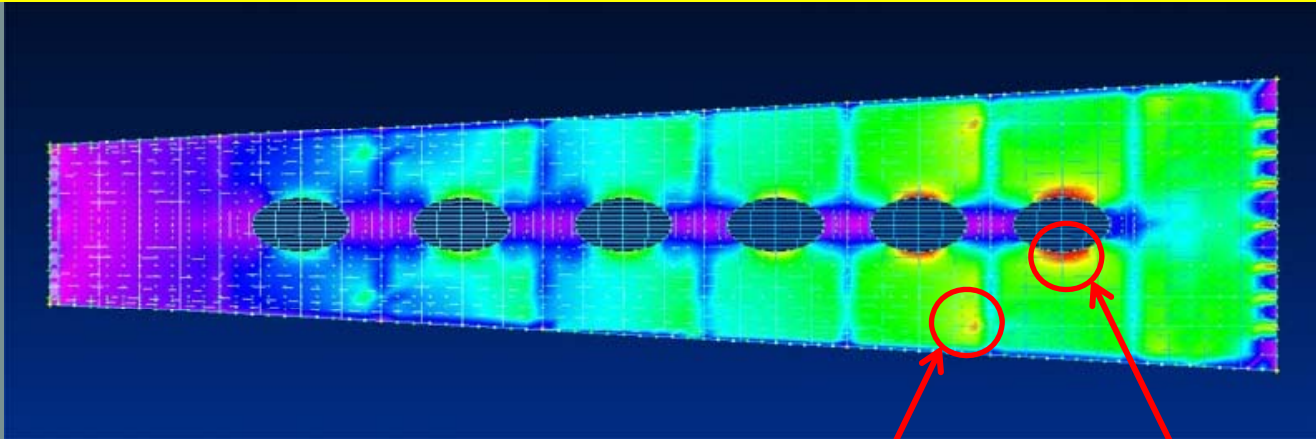


**Photo of Static Load Test  
(100%)**

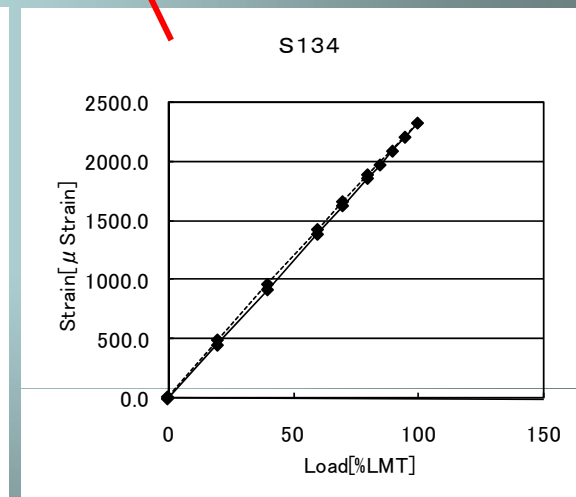
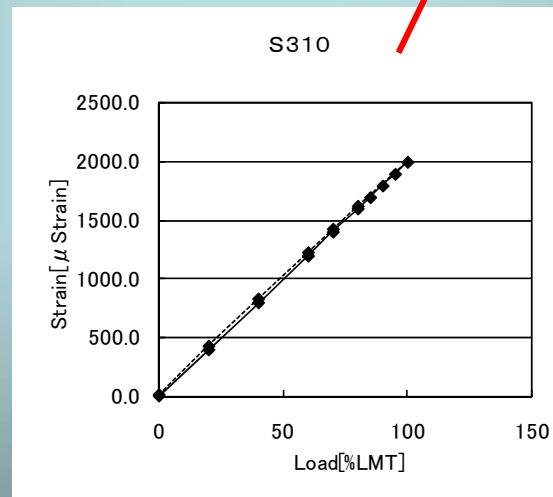
**Two life fatigue test  
of this box was  
finished**



# Comparison of calculated (FEM) and experimental strain level at limit load test [at lower panel]

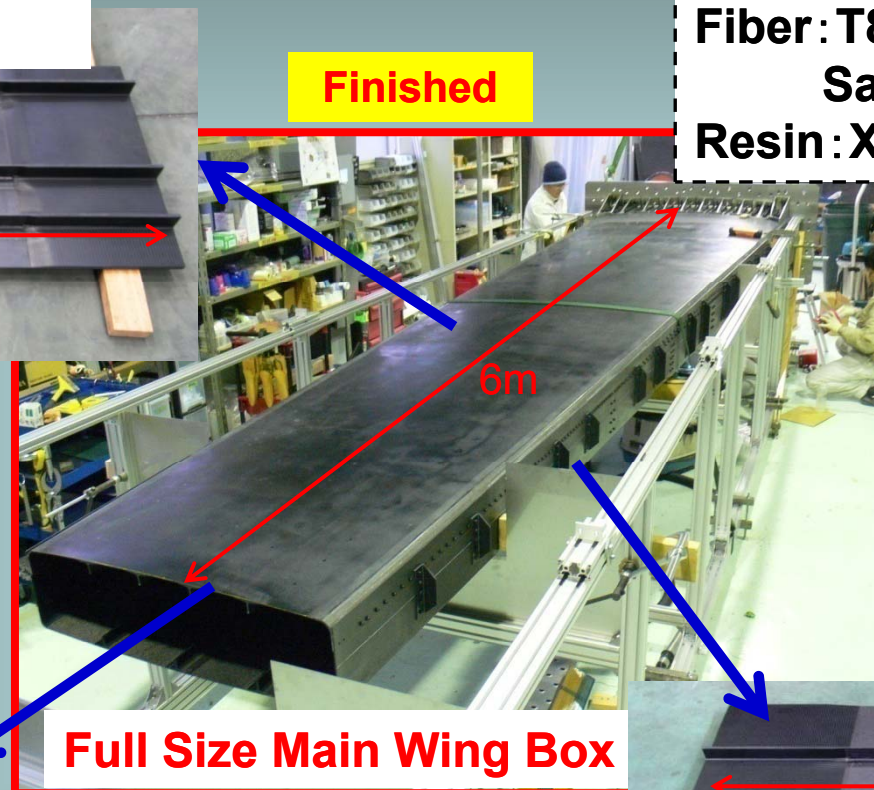
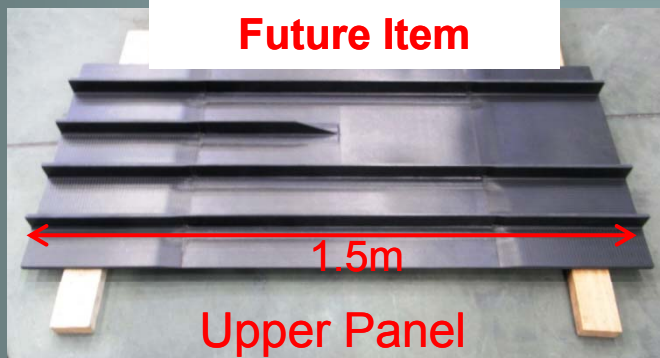


	<b>S310</b>	<b>S134</b>
FEM	2006	2260
Measured	1990	2331
Error [%]	0.8	3.0

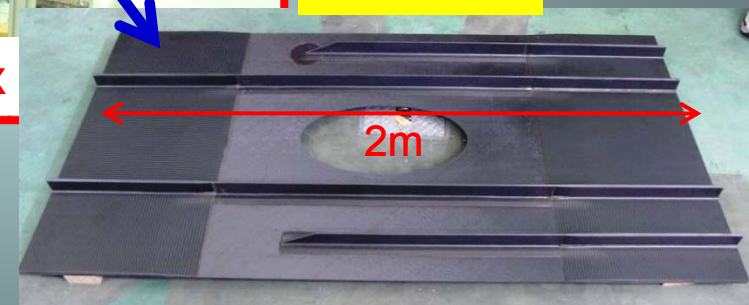
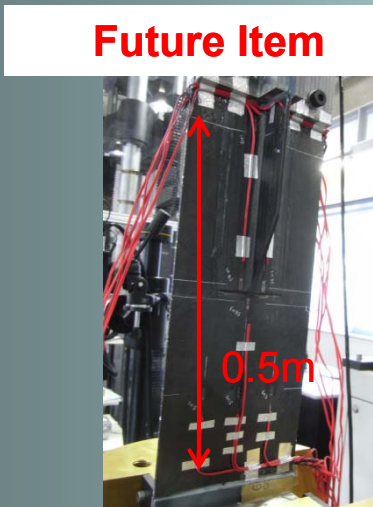


**Easy Work before the Progressive Failure  
: in Design Limit Load Test**

# Fatigue Test of VaRTM Structure : Specimens



**Fiber: T800SC-24k (Skin)**  
**Saertex NCF (Stringer)**  
**Resin: XNR6809**



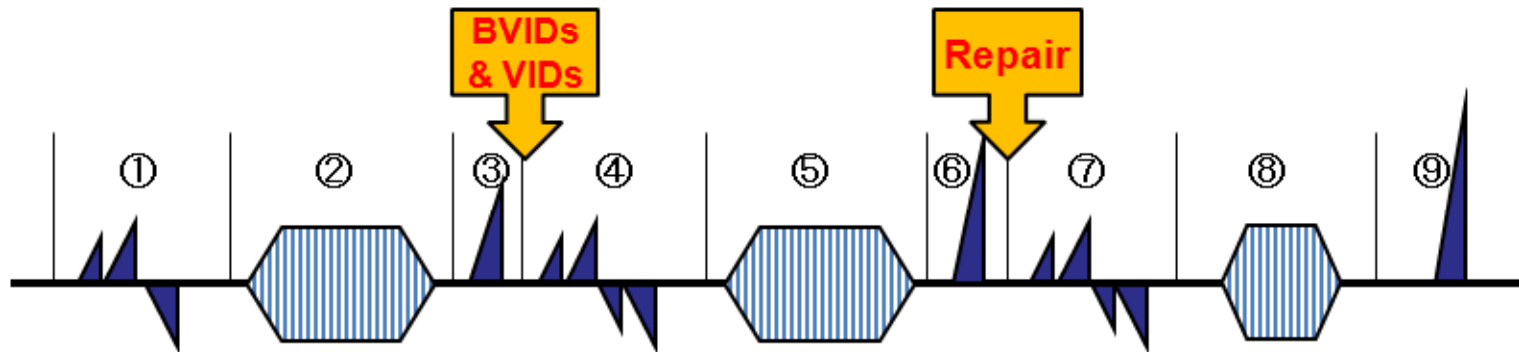
Element of Stringer Run-out

Lower Panel: Sub-component of Wing

From this slide, an early example of “Virtual test”



# Fatigue Test of VaRTM Structure: Test Plan



- ① Initial strain survey
- ② **Fatigue spectrum – 1 DSO with LEF=1.18, Life factor = 1.0**
  - Evaluate **disbonding of stringer run-out**
- ③ 100% DLL Verification
- ④ Strain survey (static behavior of BVIDs, VIDs)
- ⑤ **Fatigue spectrum – 1 DSO with LEF=1.18, Life factor = 1.0**
  - Evaluate **impact damage growth and disbonding of stringer run-out**
- ⑥ 150% DLL Verification
- ⑦ Strain survey (effects of repair part)
- ⑧ Fatigue Spectrum- 2 inspection Intervals with LEF and Life factor
  - Evaluate **DT of repaired part**
- ⑨ Destruction Test

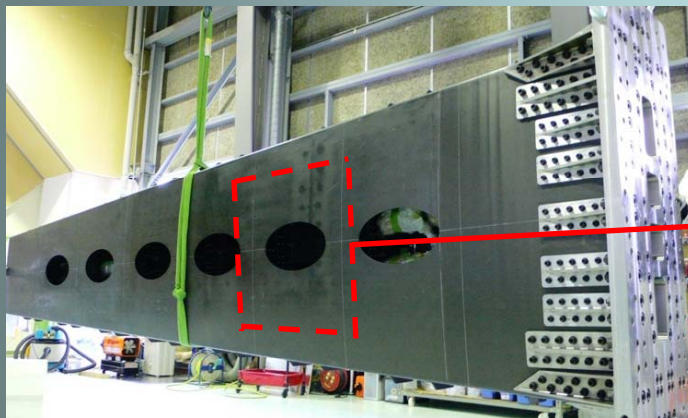
DSO: Design service objective

LEF: Load enhancement factor (Considering Scatter of Fatigue Strength)

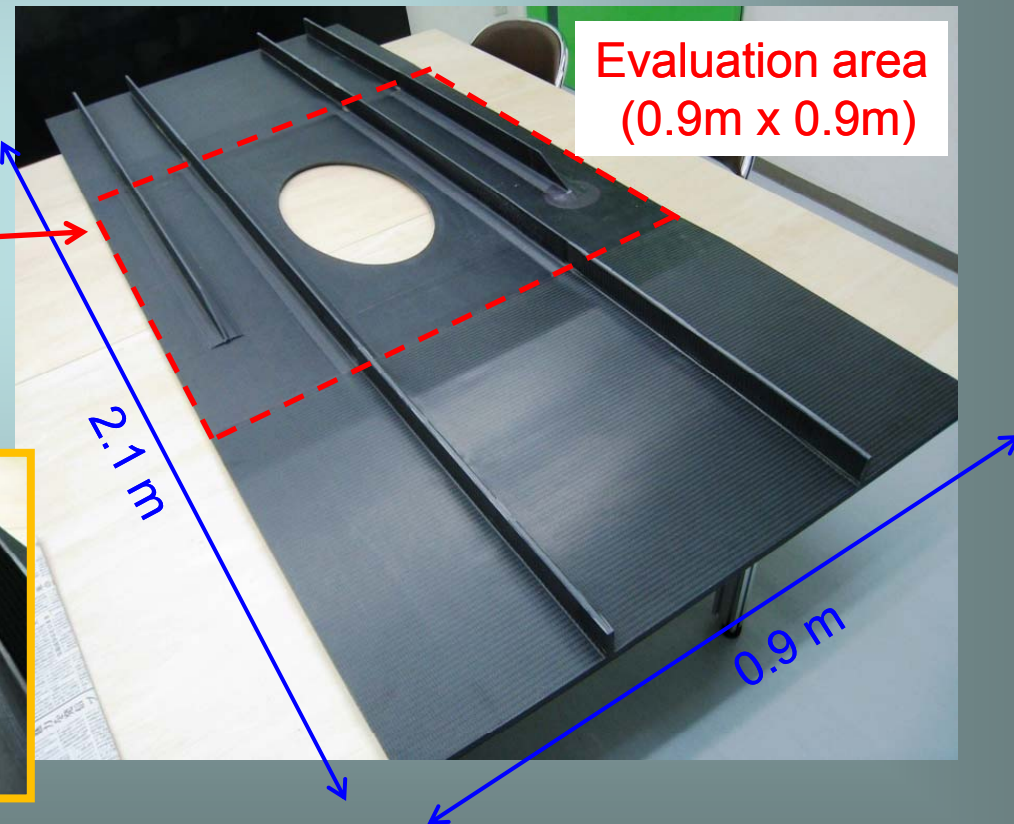
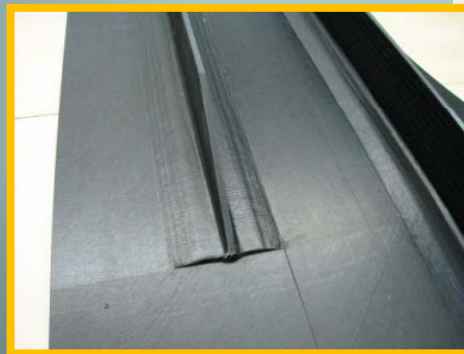
DLL: Design limit load

# Fatigue Test of VaRTM: Lower Panel as Sub-component of Main Wing

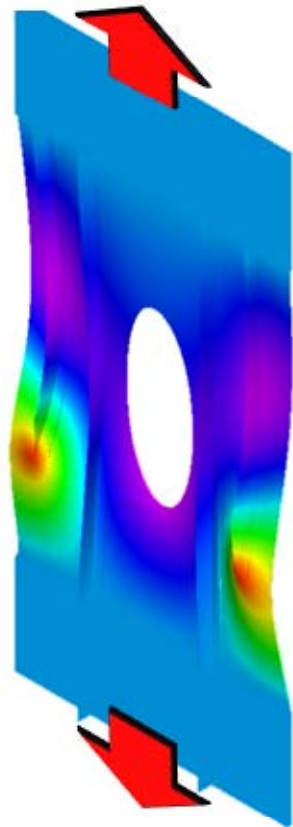
- Dimension: 2.1m in Length x 0.9m in Width
- Critical Portion: Edge of Stringer Run-out, Maintenance Hole



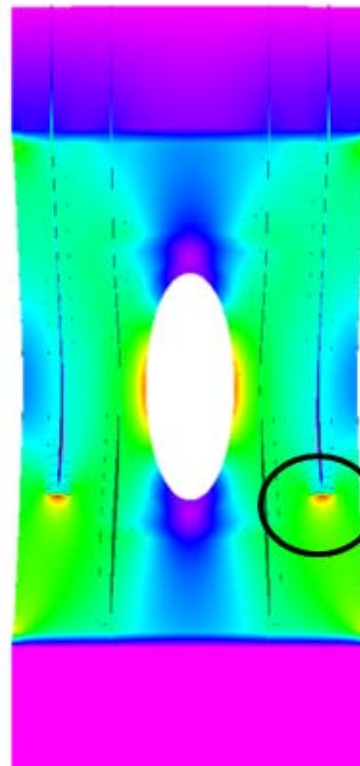
Region of  
interest:  
Stringer  
run-out



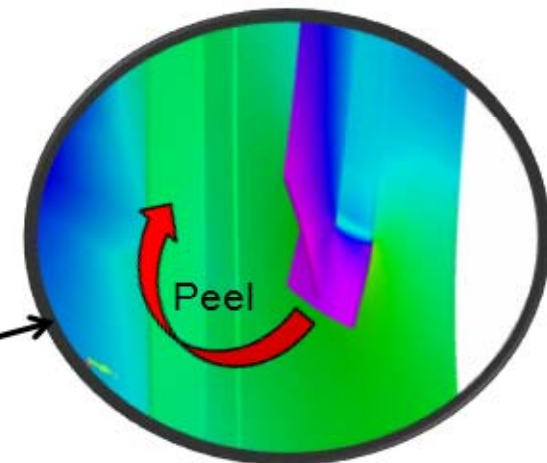
# Fatigue Test of Lower Panel: Pre-test Analysis for Static Tension



Out-of-plane displacement



Principal strain



Disbond

## Design Strain (@100%DLL) ← OHT Critical

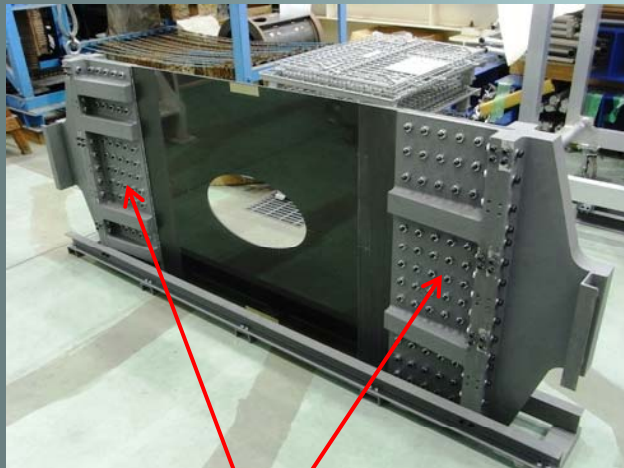
- Stringer: 2,200 $\mu$
- General Skin: 2,300 $\mu$
- Edge of Maintenance Hole: 4,000 $\mu$



Designed for the most critical in-plane strengths to load conditions (environment factor: considered)

# Fatigue Test of Lower Panel: Preparation Procedure

- Fitting of Steel Loading Fixture to 2 Ends
- Loading: 2,500kN High Speed Actuator (MTS)
- Strain Channels: 76,  
Deflection Measurement Points: 4
- 3-D Optical Deformation Measurement (DIC)

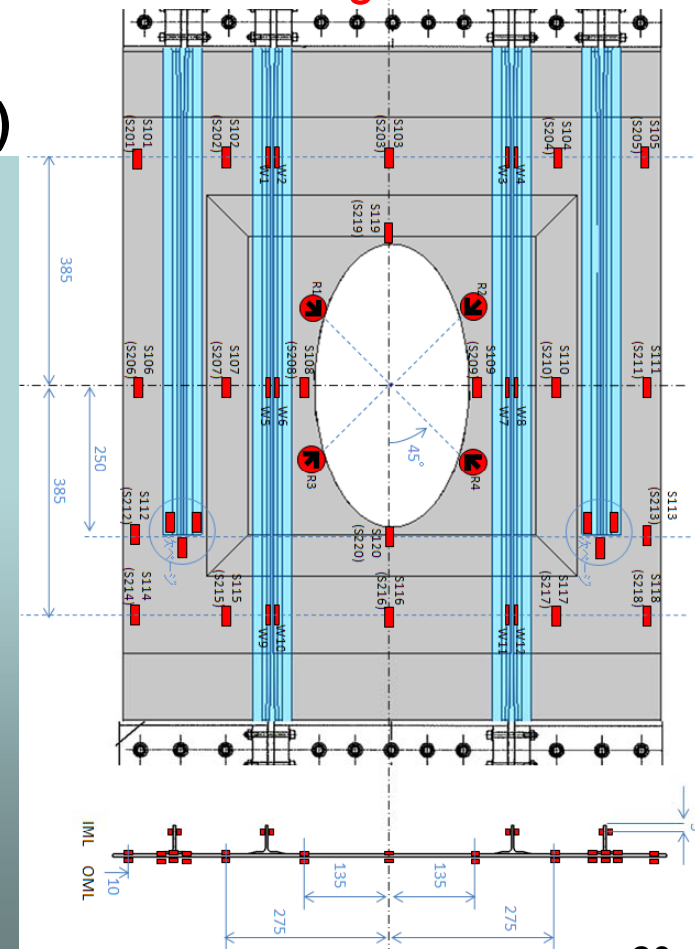


Fitting by Bolts and Adhesion



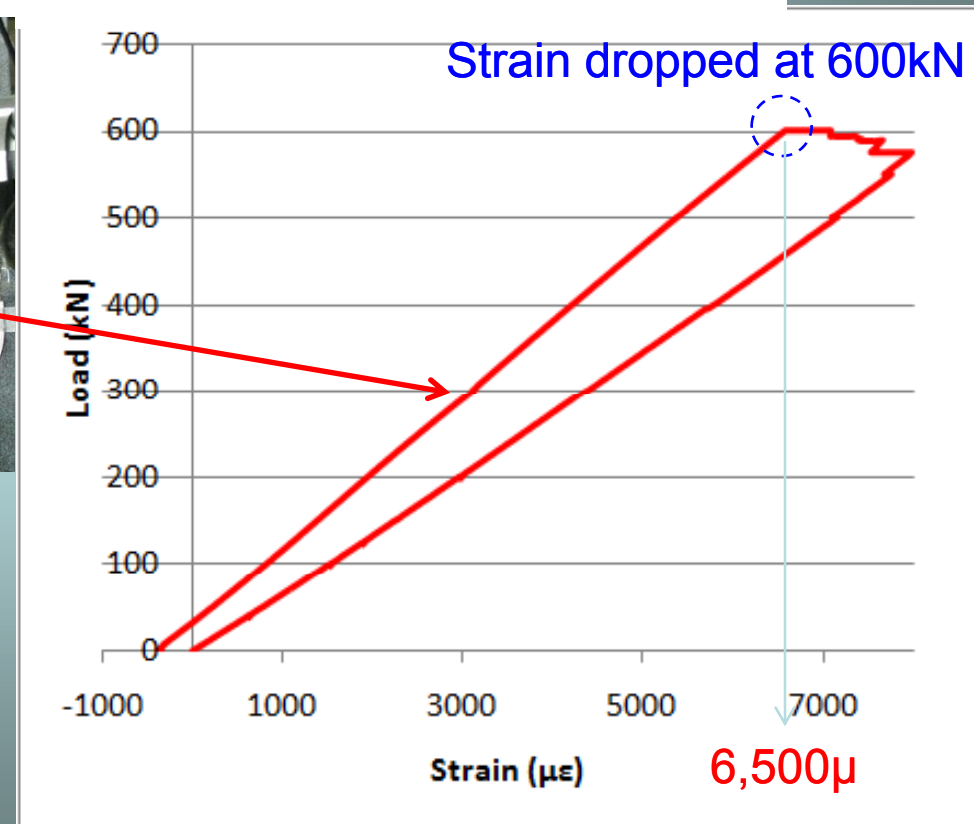
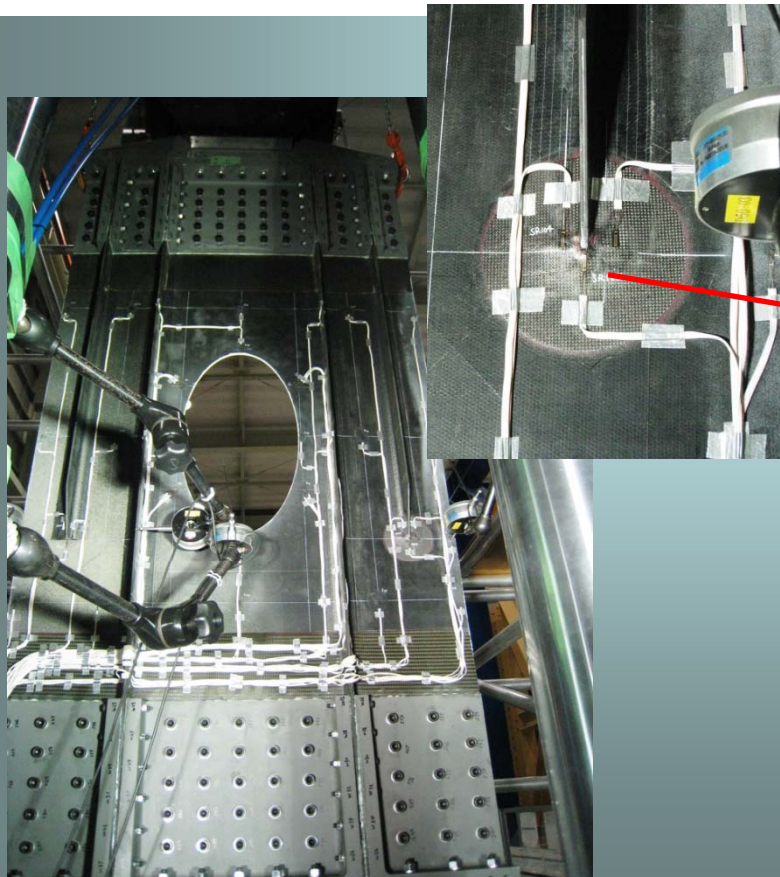
2,500kN Machine

## Strain Gage Locations



# Fatigue Test of Lower Panel: Strain Survey as the 1<sup>st</sup> Step

- Initial Adaptation of Fixture, Check of Measurement System, Comparison with Analysis
- **Bestowment of Initial Damage at Edge of Stringer Run-out**
  - ⇒ Created at 82% DLL: Peel Force by Local Bending
  - ⇒ No Detrimental Residual Deformation

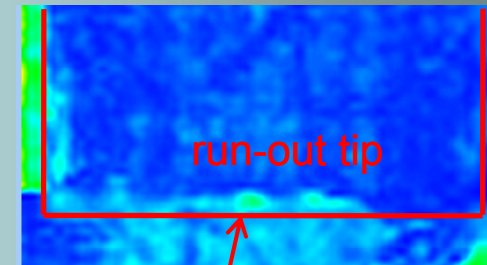


# Fatigue Test of Lower Panel: Inspection after Strain Survey

- Non-Destructive Inspection by Using Array Probe Ultrasonic C-Scan  
⇒ Small Delamination at Tip of Stringer Run-out (5mm x 2mm)



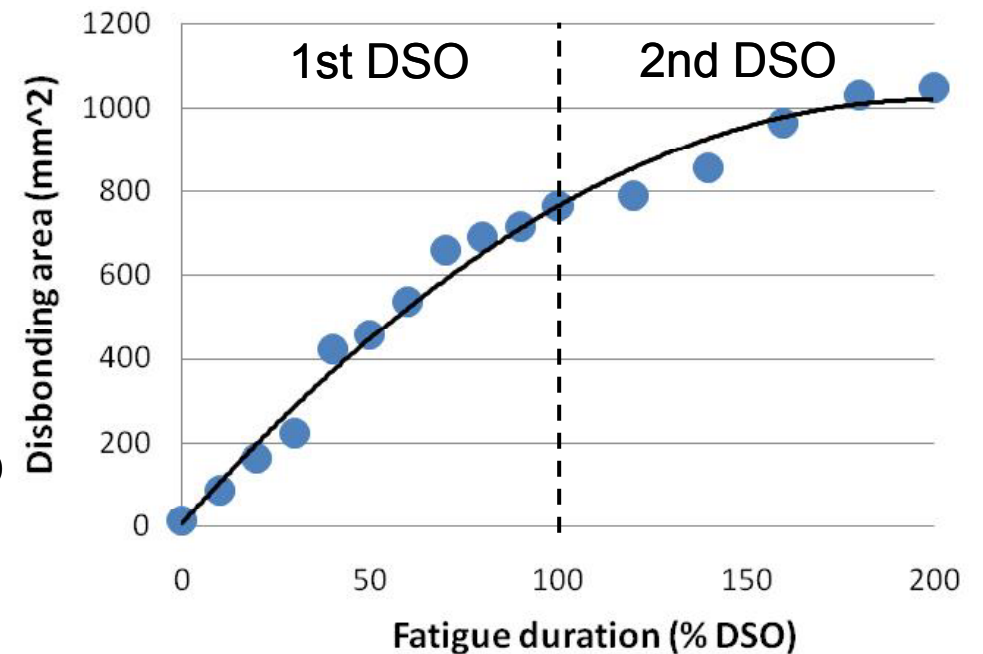
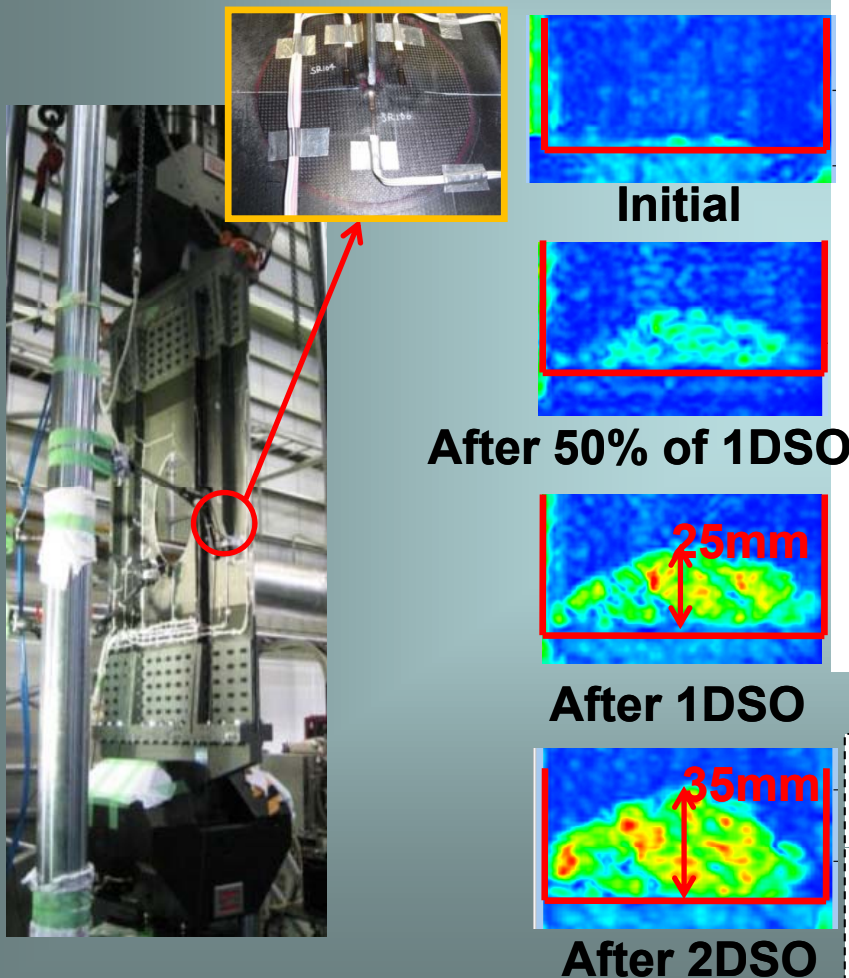
64ch x 5MHz linear  
array sensor



Disbonding (5mm x 2mm)

# Fatigue Test of Lower Panel: Evaluation of Delamination Growth

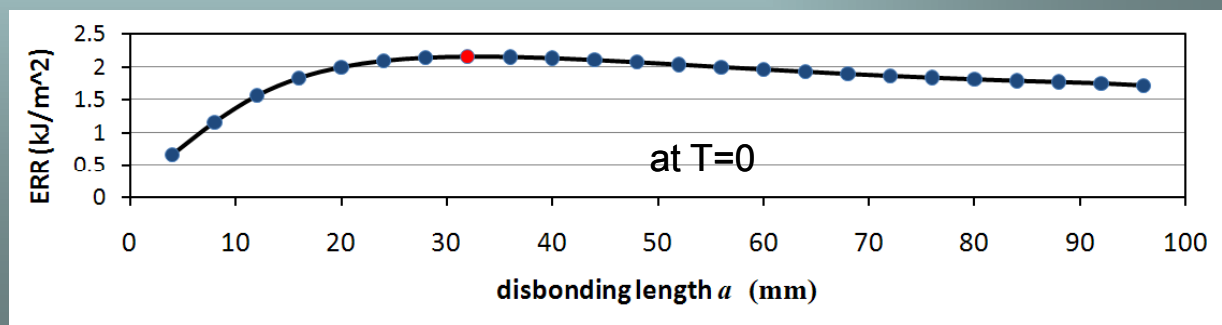
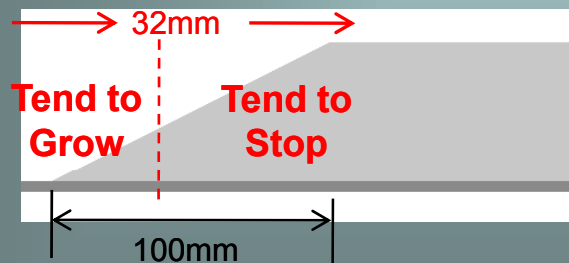
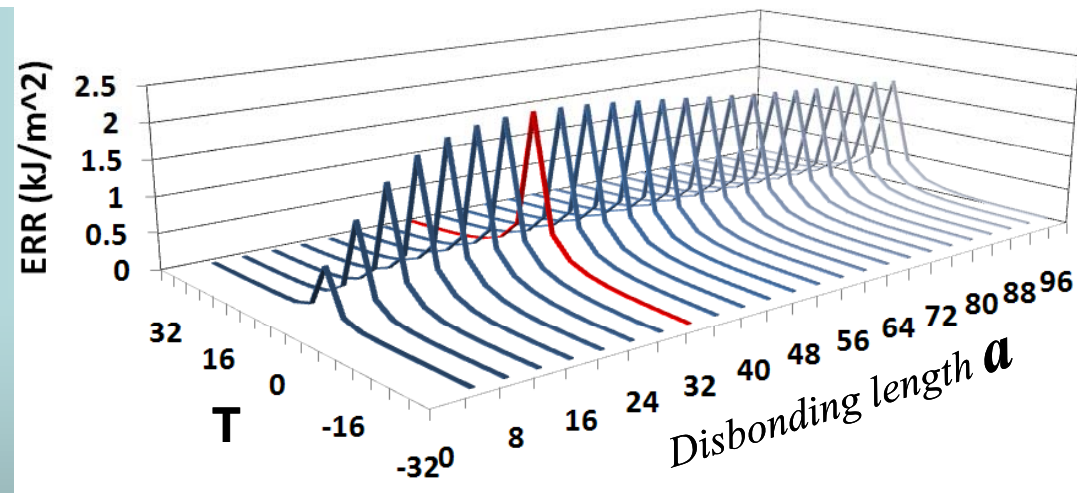
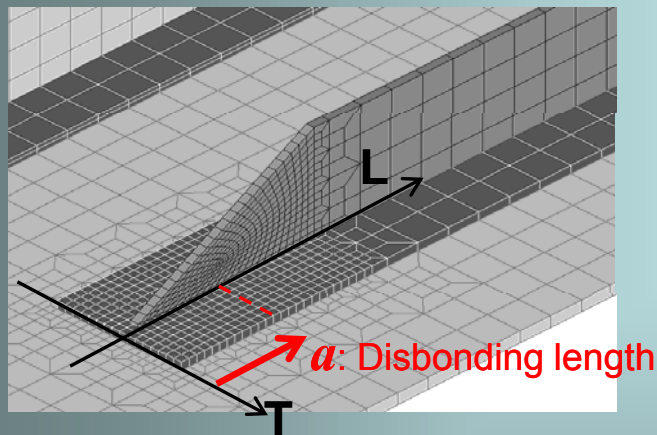
- Inspection Interval: at Every 4,000 Flight (every 10% of DSO)
  - By Human Eye: No Finding
  - NDI: Growth of Delamination at Stringer Run-out Tip



- Stable Growth during 1 DSO (slow growth)
- No Effect on Whole Structural Integrity at 100% DLL Test after 1 DSO

# Fatigue Test of Lower Panel: Numerical Analysis of Damage Growth

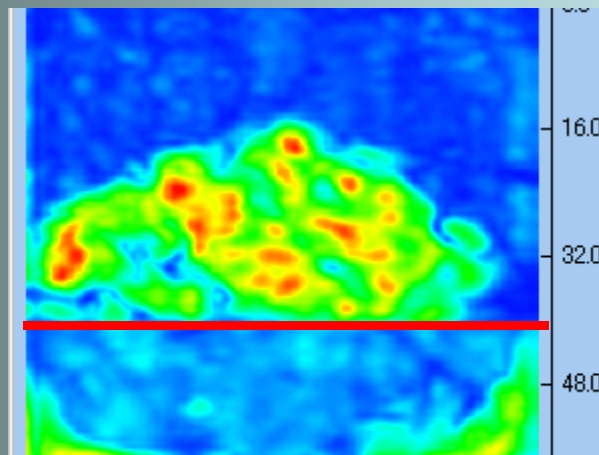
- Obtained Relationship between Delamination Length  $a$  and Energy Release Rate Distribution at Tip  $\Rightarrow$  Mode I Dominant ( $G_I \gg G_{II}, G_{III}$ )
- Energy Release Rate Distribution
  - Width-wise (T): Maximum at the Center(= below Web)
  - Length-wise (L): Increase within  $a < 32\text{mm}$   $\rightarrow$  Tend to Grow  
: Decrease over  $a > 32\text{mm}$   $\rightarrow$  Tend to Stop



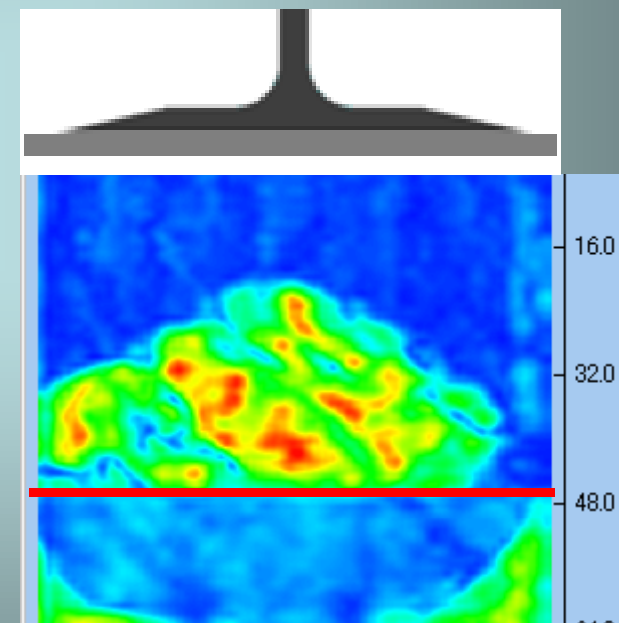


# Fatigue Test of Lower Panel: Damage after Ultimate Load Test

- Loading to 150% DLL, Keep for 3 Seconds
- Slight Growth of Delamination at Stringer Run-out, No Finding other Detrimental Residual Deformation or Rigidity Reduction
- No effect on Structural Integrity



Before 150% DLL test



After 150% DLL test

If numerical prediction is successful, this test can be eliminated.  
Current simulation level: not 100% complete, future task

# Research of Lightning Strike to Aircraft Composite Structure: Background



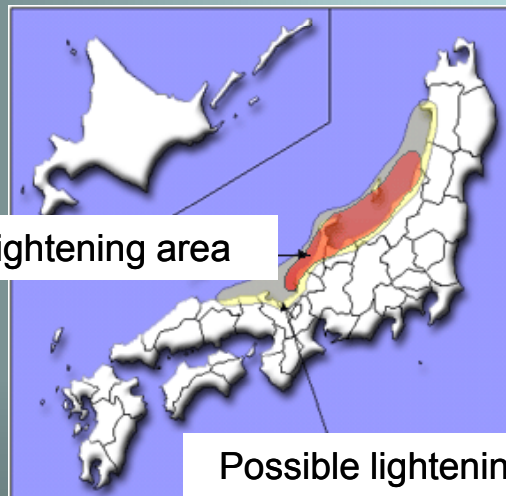
**Increase** of CFRP application: **Main wing**

Topics

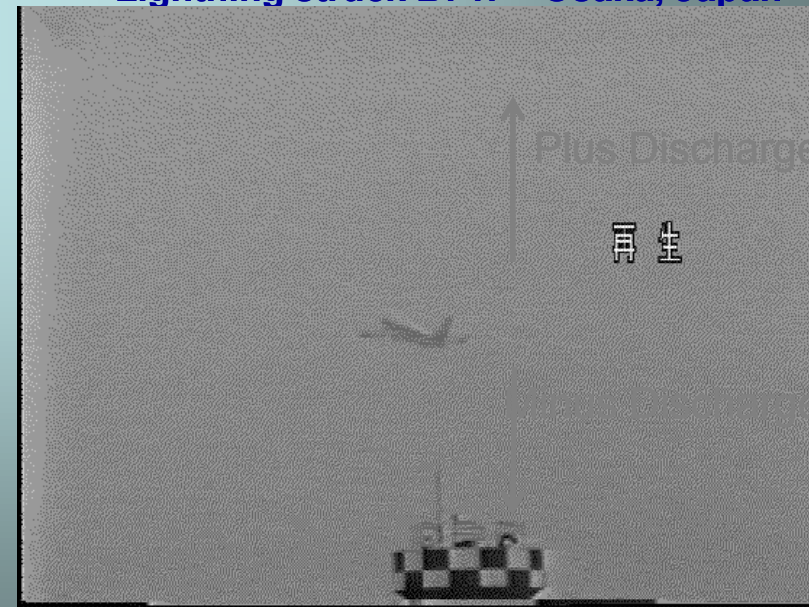
- Damage mechanism by lightning
- Residual strength and durability after strike
- Method of repair/ strength after repair
- **Spark problems in integral fuel tank**

Japan Sea coast line in winter:  
Meteorological anomaly

➡ **High energy, frequent lightning**



Lightning struck B747 Osaka, Japan



Courtesy of website of Dr. Kawasaki  
(Osaka Univ.): (<http://zenk.sblo.jp>)

# Simulated Artificial Lightning Test

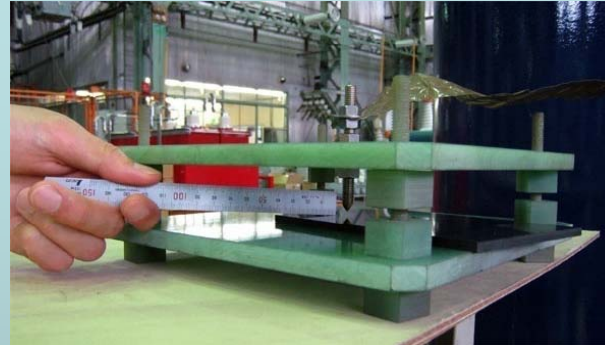
## Final Goal: Elimination of Costly Test

Lightening Strike to Regular Compression after Impact Specimen



**High Voltage Impulser, by HAEFELY Co.  
(Owned by Nisshin Electric Co. Ltd [Japan])**

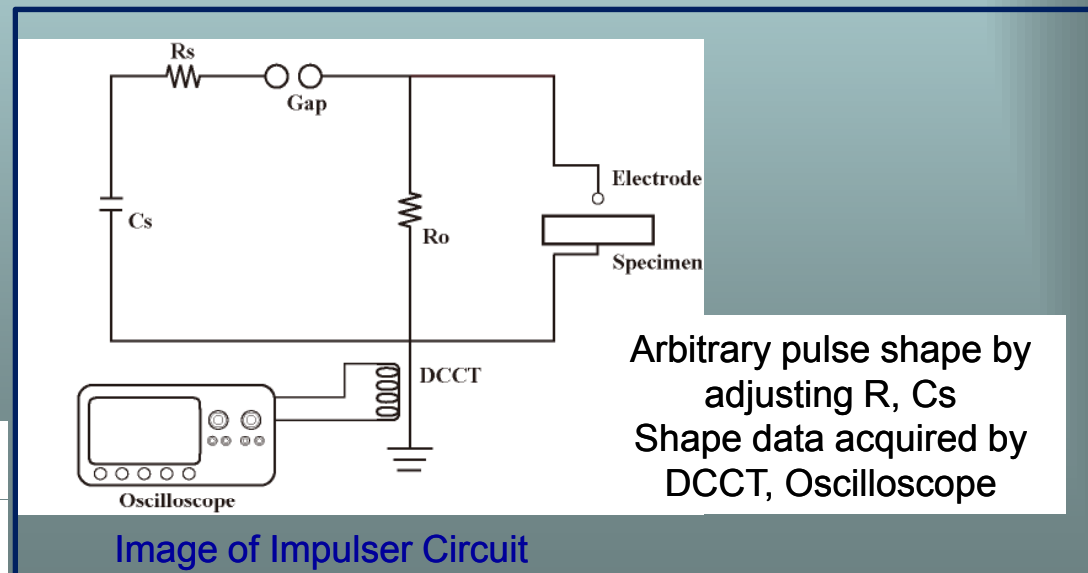
Maximum capability: 2400kV 120kJ  
 Time Parameter for Impulse Current Pattern:  
 4/10 $\mu$ s, 8/20 $\mu$ s, 0/350 $\mu$ s  
 Maximum Current:  $\pm 40$ kA ( $\pm 20$ kA)



Fixture for specimen

**Specimen**  
 ASTM D7131 (CAI)

IM600/133  
 [45/0/-45/90]4s (n=4)  
 t = 4.7 [mm]  
 100 × 150mm



# Lightening Impulse Test Parameters



## Discharge condition

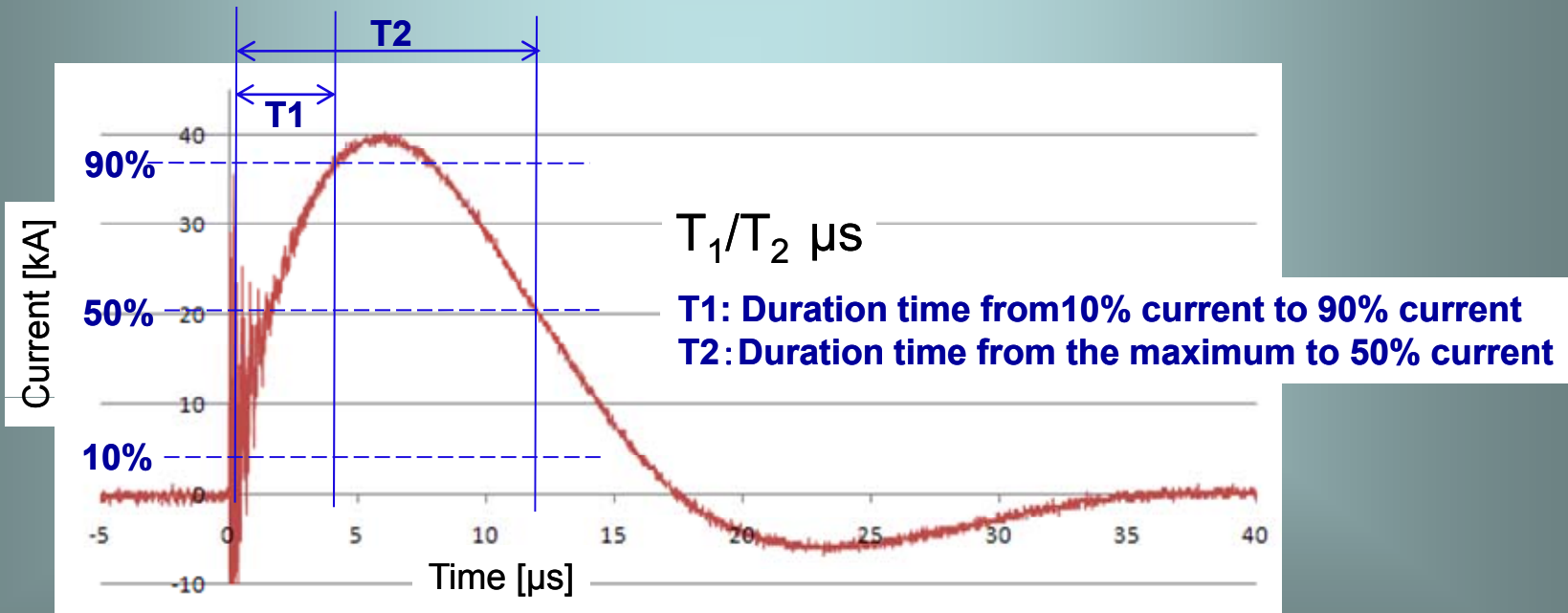
	Waveform [μs]	Peak Current [kA]	Electrical Charge [C]	Action Integral [A <sup>2</sup> s]
I		20	0.20	2831.38
II	2.6/10.5	30	0.31	6273.28
III		40	0.41	11440.90
IV		20	0.42	5444.82
V	4/20	30	0.63	12350.97
VI		40	0.82	20887.35

Electrical charge

$$Q = \int i dt$$

Action Integral : AI  
(Specific current energy)

$$AI = \int i^2 dt$$



Obtained impulse current shape at simulated lightning test(4/20, 40kA)

# Observed Damage Geometry

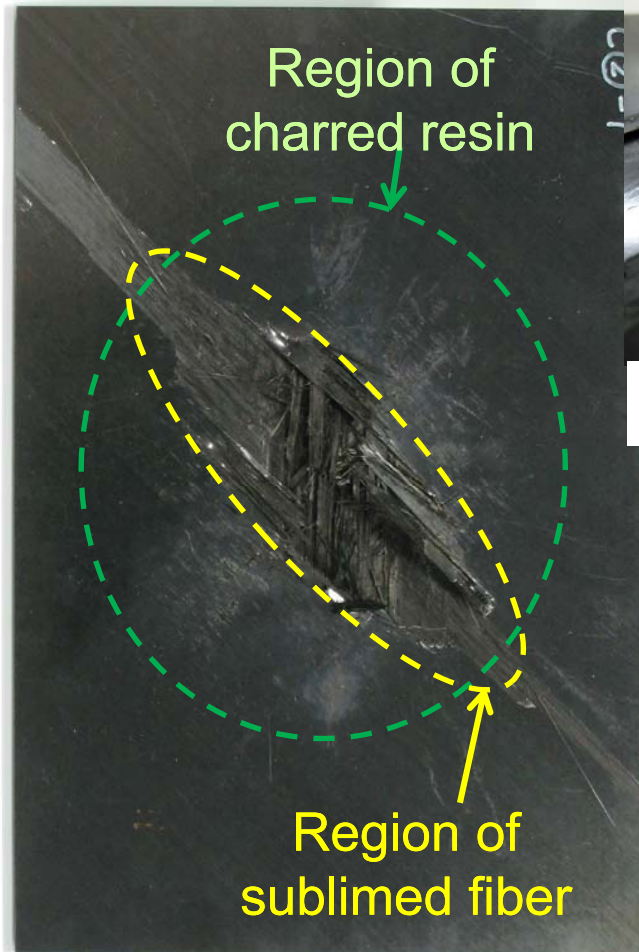


Photo of damaged specimen



Vicinity of impulse contact point

Wave profile : 4/20 $\mu$ s  
Peak current : 40 kA  
Action Integral :  $2 \times 10^4$  [A<sup>2</sup>s]  
thickness : 4.7mm

## Observed two damage modes

- Surface damage
  - Sublimation of fibers in some plies
  - Delamination under surface ply
- Charred or sublimed resin: circular area

**Estimated scenario: Created super high temperature by Joule heat due to high electric current**

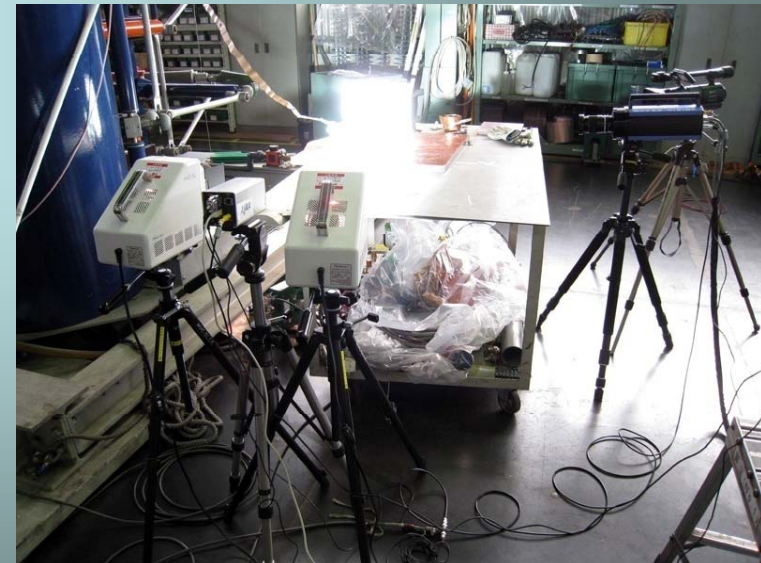
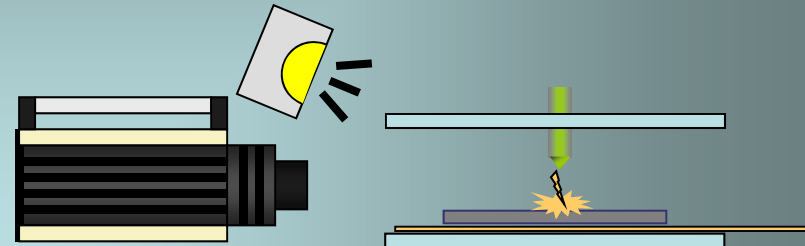
**⇒ Explosive sublimation of fiber or resin**

# Understanding of Mechanism by Using Ultra-High Speed Video



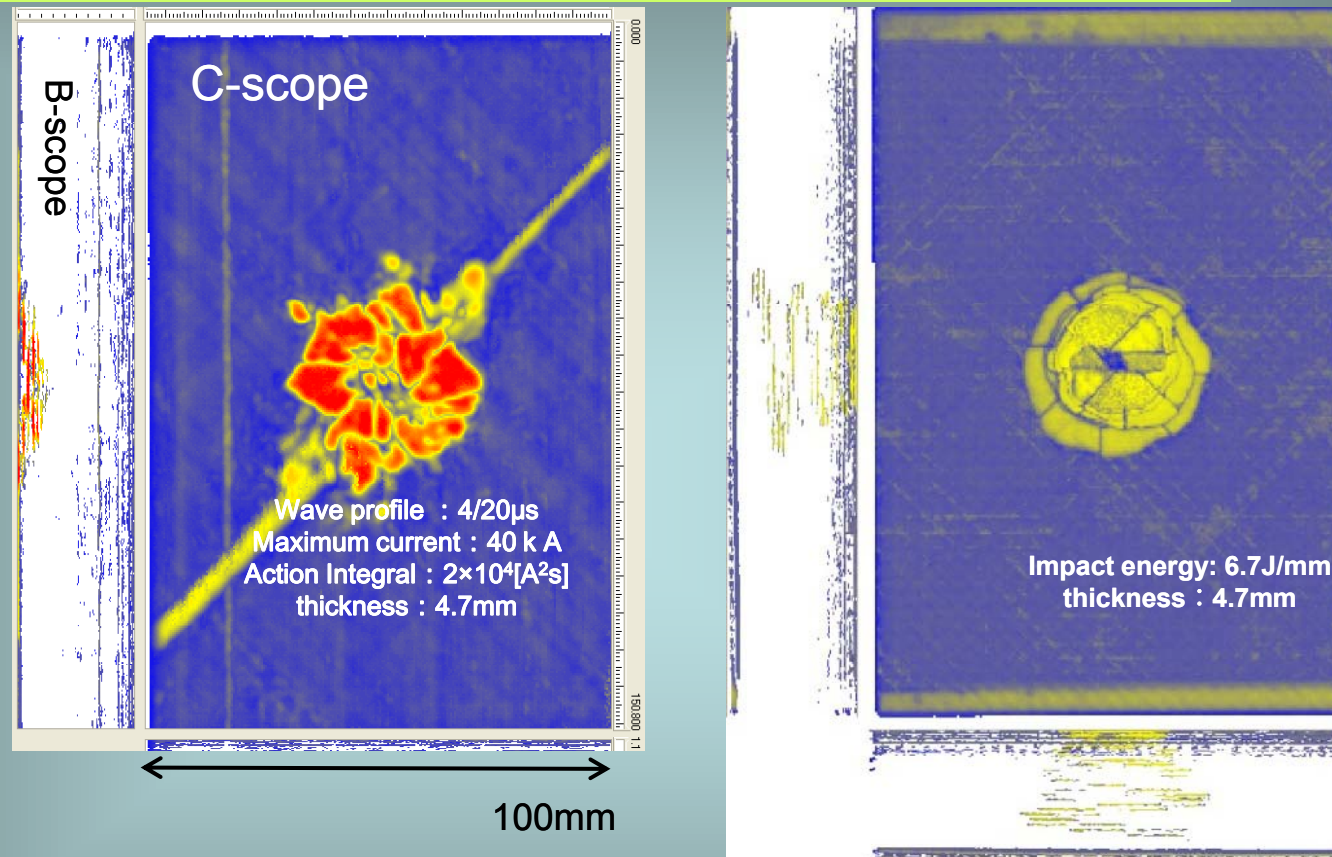
Wave profile : 7/150[ $\mu$ s]  
Max. current : 20[kA]  
Action Integral (AI) :  $3 \times 10^5$ [A<sup>2</sup>s]  
Thickness : 4.7[mm]

High-speed camera by Shimadzu Co. Ltd  
HPV-1 (1,000,000fps max.)



Frame rate : 500,000 fps  
Record duration : 200  $\mu$ s

# Internal Damage Pattern by Ultrasonic C-scan



	Damage by lightning	Damage by mechanical impact
Delamination	Delamination between each ply: A pair of fan-like shape	
Cause of growth	Thermal & electrical anisotropy	Mechanical anisotropy
Thickwise extent	A few plies near impulse point	Whole in the thickness

# Internal Damage Pattern by X-ray CT Scan and Actual Cutting

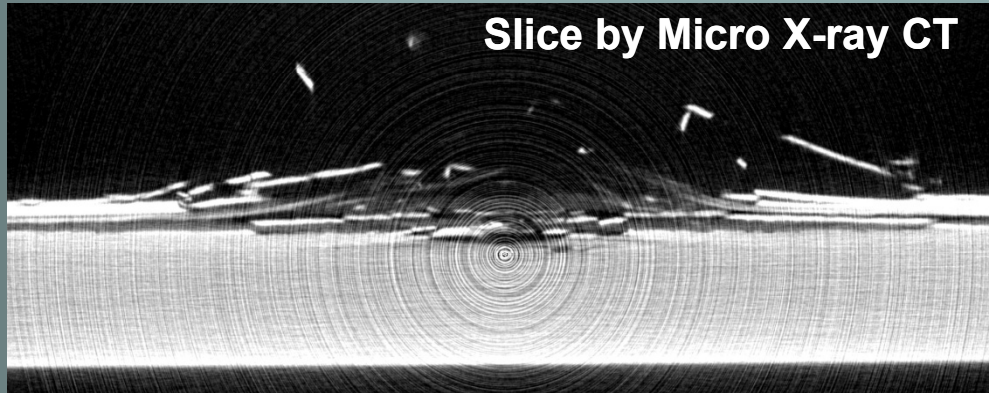
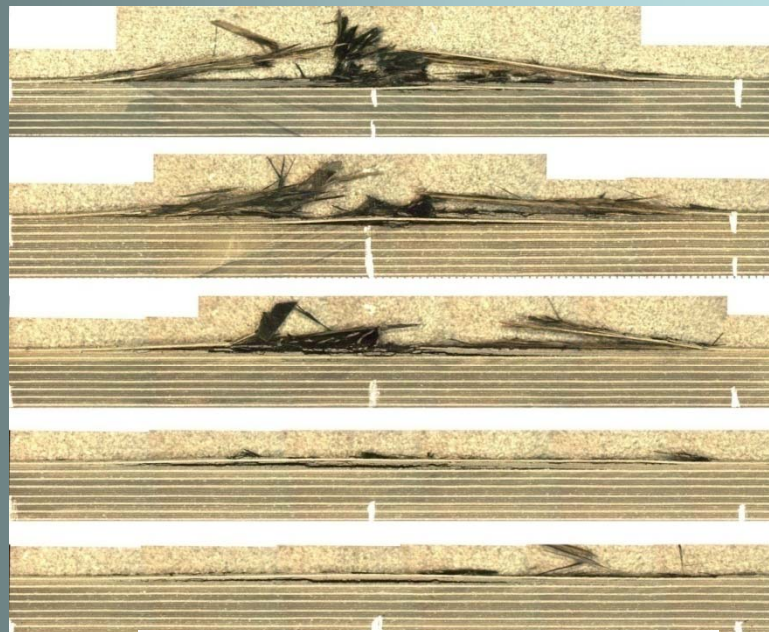
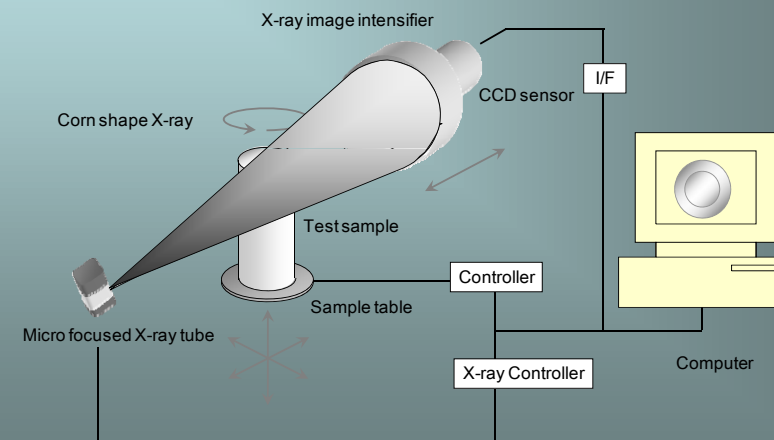


Photo of Micro X-ray CT Scanner



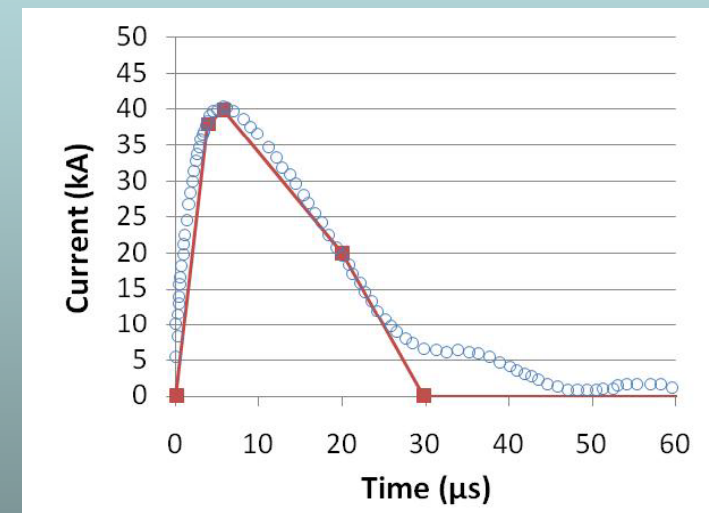
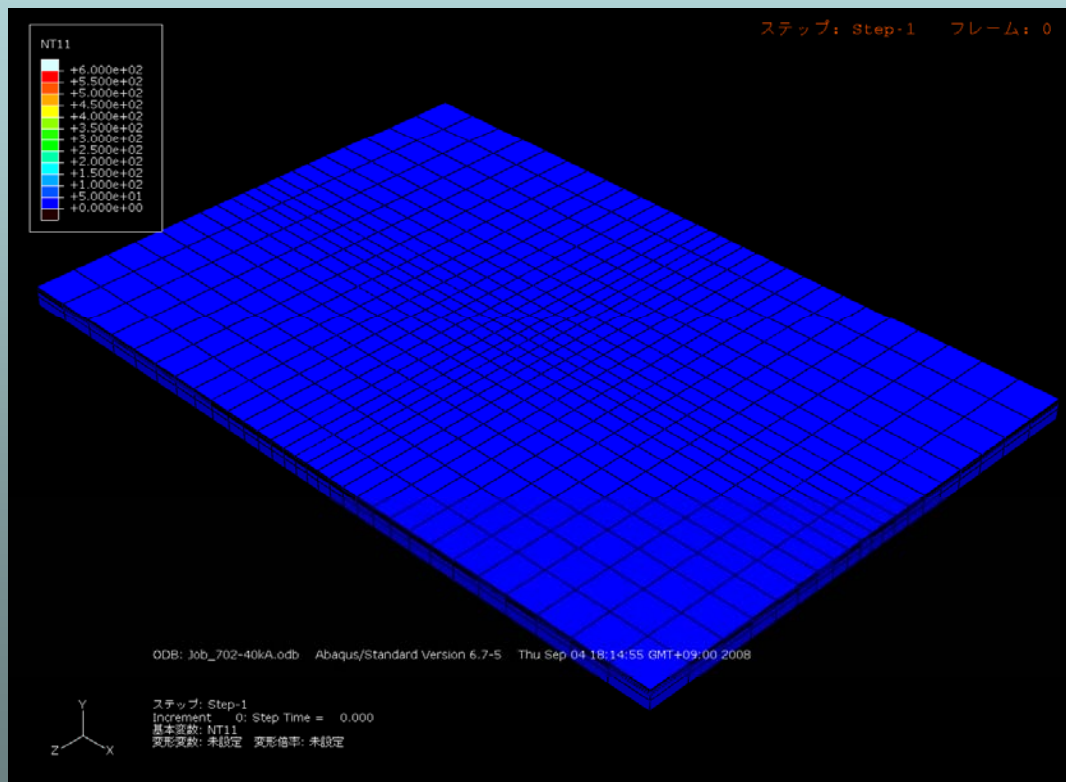
Pictures of cut sections





# Results of Numerical Temperature Simulation (During and just after Lightning)

- Peak Current: 40kA, Wave Time Parameter: T1/T2=4/20  
During Lightning: 0~30  $\mu$ sec., After Lightning: 30~50 $\mu$ sec.
- Gray Color Region Indicates over 3000°C  
(Decomposition→Delamination→Sublimation)



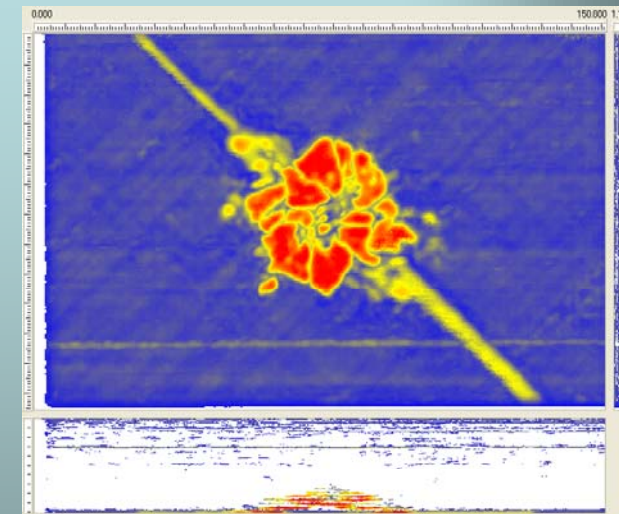
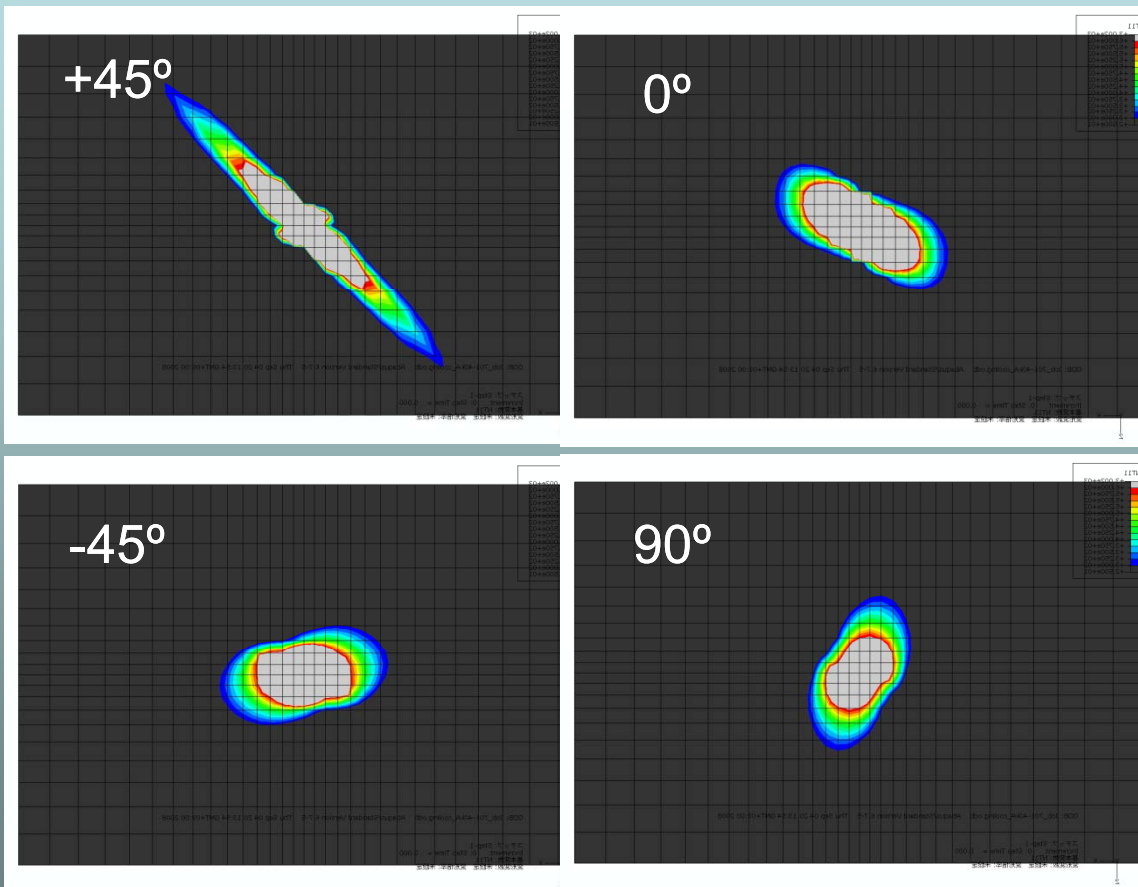
0~50  $\mu$ sec



# Temperature Distribution at Each Ply

## Current Simulation Level: Qualitative

- Peak Current: 40kA, Wave Time Parameter: T1/T2=4/20
- Regions over 300°C : Indicated
- Distribution Shape: Affected by Heat Conduction after Lightning



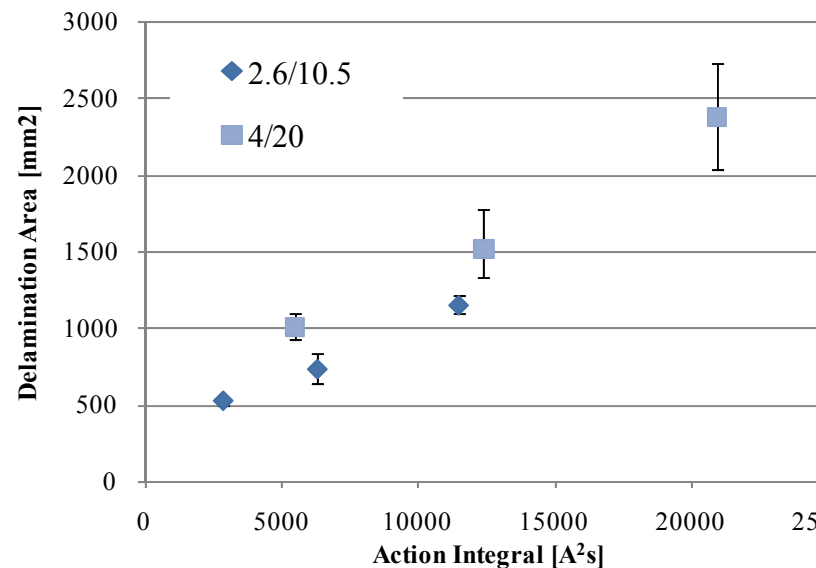
**Ultrasonic C-Scan  
from the Backside  
of the Specimen**

**Level of numerical simulation: only at a gateway**

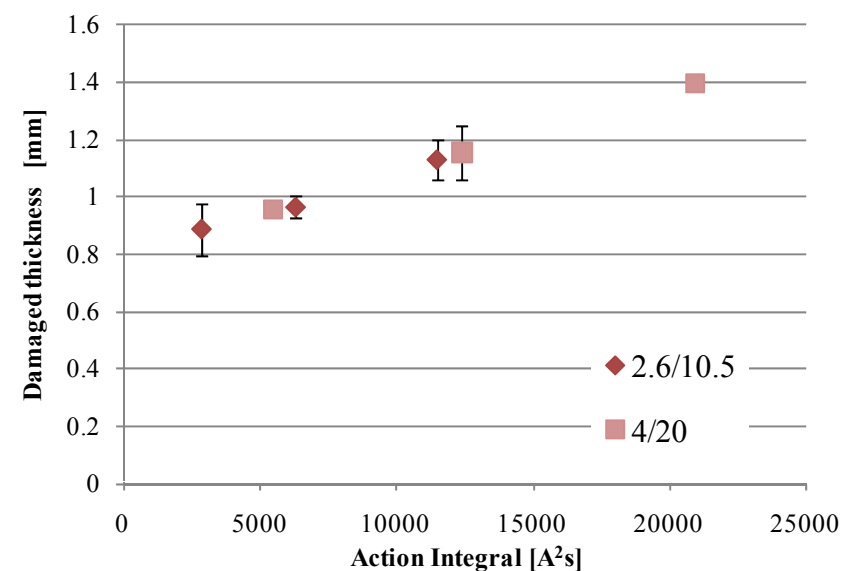
# Relationship between Lightning Energy and Damage Extent

- Delamination area (in projection)
  - Fiber damage
  - Resin char
- Damage depth (Mainly delamination)

**Next Step: More Quantitative EME Based Analysis**



**Projected delamination area vs AI**



**Damage depth vs AI (by Micro CT)**

**Almost linear relationships between AI (Specific current energy) and delamination area and AI and damage depth**

# Summary



- Increase of composites percentage in aero-structures
- Recent two major challenges: B-787 and A350
- Precious lessons learned: Delay and cost issues, Unexpectedly low weight reduction, increase?
- Proposal for Development Cost Reduction  
Substitution of some steps in BBA by “Virtual testing”  
“Virtual processing” : Out of scope, today
- Example: Lower panel of VaRTM wing test, potential of future substitution of BBA steps by simulation
- Example: Lightning strike damage: difficult & costly tests, at a gateway of accurate numerical simulation
- If high development costs remain in composites, aircraft industries may go back to aluminum again!